



Bruce Ohme and Mark R. Larson  
bruce.ohme@honeywell.com  
Honeywell Aerospace  
Plymouth, Minnesota USA

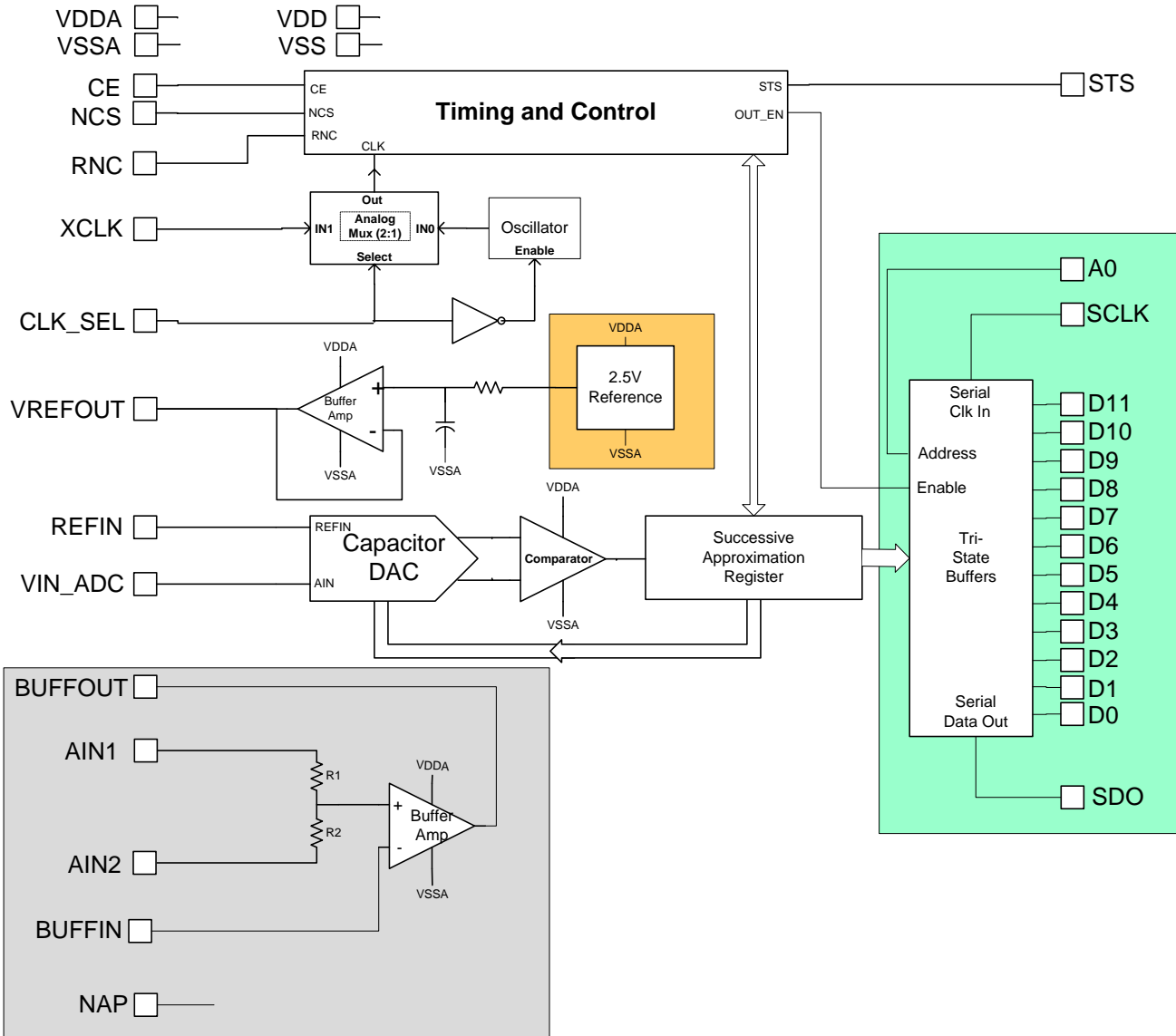
# High Temperature Analog to Digital Converter Reliability Testing

**Honeywell**

## HTADC12 - High Temp 12-Bit ADC Reliability Study

- **It is common practice to characterize and compensate initial measurement errors in down-hole tools**
- **Component drift over time and temperature cycling are therefore just as important to know/predict as time-zero accuracy**
- **Parametric shifts affecting post-compensation accuracy are presented for a 12-bit ADC from samples stressed by 250°C bias plus temperature cycling from -65°C to 200°C**
- **Mechanical / Assembly data is also presented**

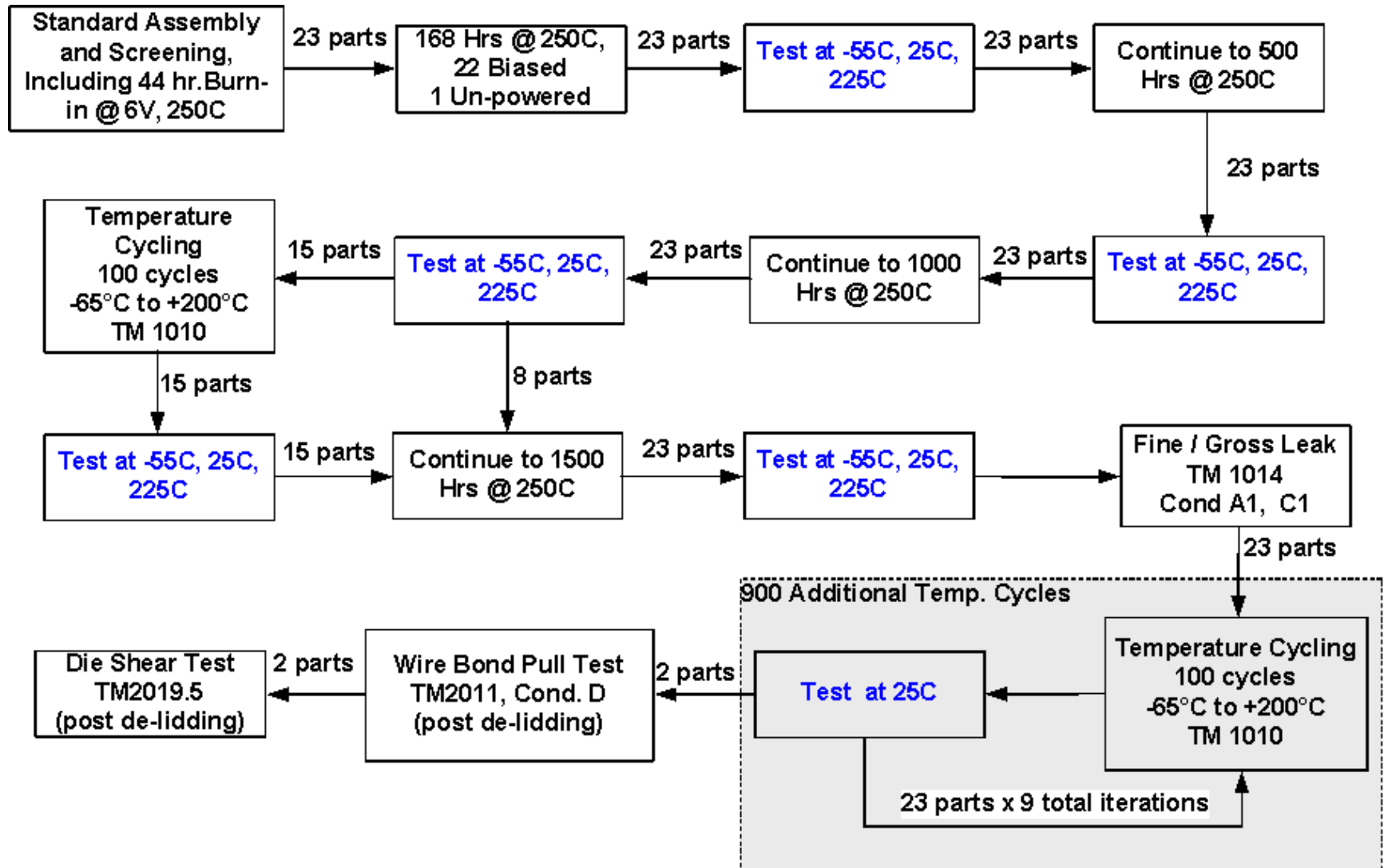
# HTADC12 Block Diagram



- **12 Bit Successive Approximation ADC**
- **Temperature range: -55°C to 225°C**
- **5V supply: 0V to VREF full-scale input range**
- **On-chip 2.5V Reference**
- **On-chip buffer op amp**
- **4MHz internal clock for conversion**
- **10µs conversion time**
- **Parallel or Serial data outputs**
- **28 or 14 pin DIP package configurations**

# Life-test/Temp-Cycle/Test Flowchart

## 1500 Hours at 250C + 1000 Temp-cycles (-65°C to 200°C)



# Assembly Details

- **Ceramic 28-lead DIP package**
  - Multi-layer alumina ceramic
  - Kovar lid / Furnace seal
  - Alloy 42 side-brazed leads
  - Gold over nickel surface metalization
- **Gold-backed SOI die**
  - Die-size = 2.8mm x 2.9mm
  - Aluminum wirebond pads
- **Gold-eutectic die bond**
  - Gold (1% Si) die attach preform
- **Aluminum ultra-sonic wedge bond**
  - 1.25 mil aluminum (1.5% Si) wire



*14-lead package uses similar materials/flow*

*Current production uses high-temp. adhesive die-attach*

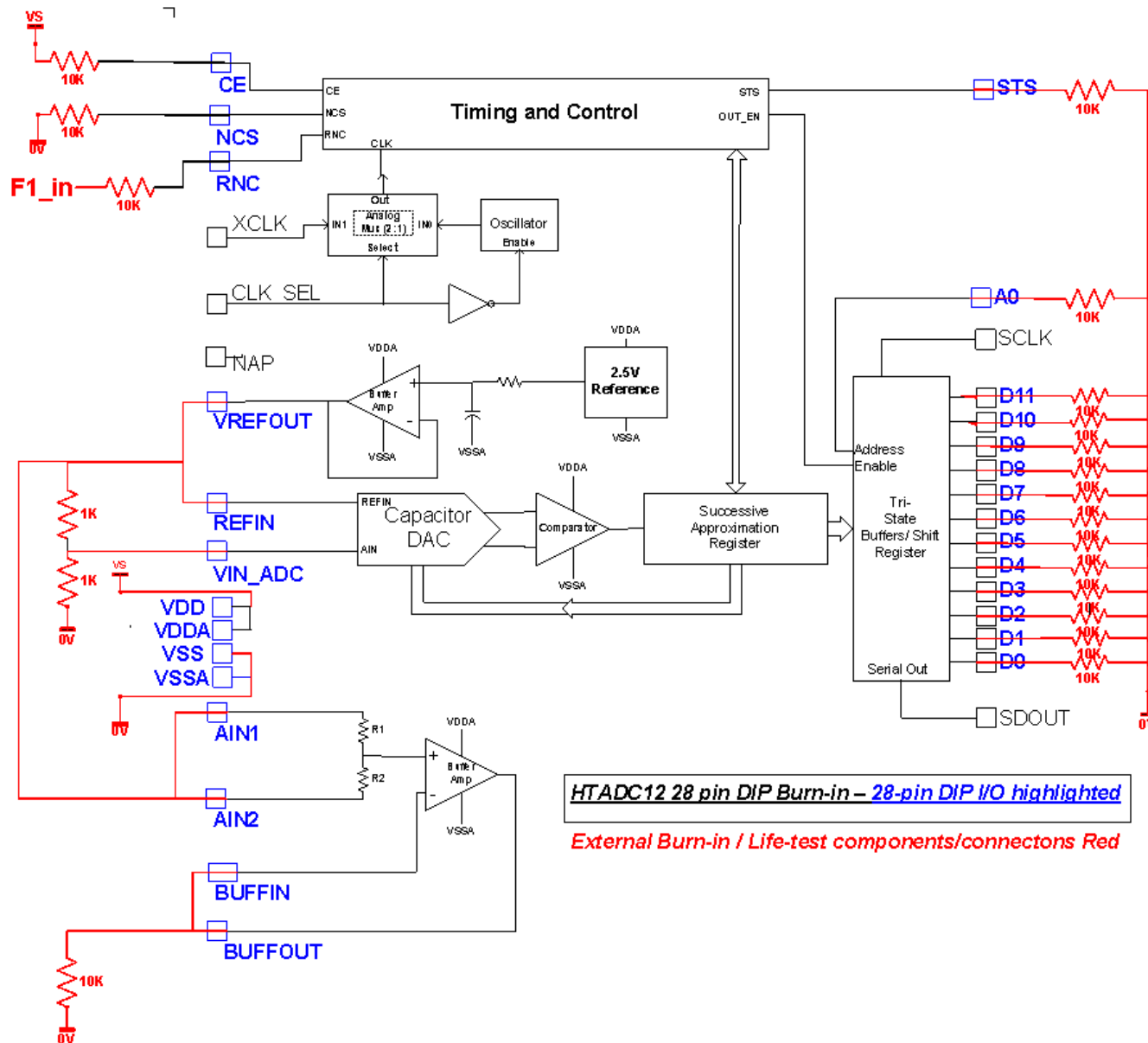
# Life-test Fixture

- High-temp. sockets mounted on aluminum rails.
- Wire-wound resistors
- Nickel wire/Fiberglass sheath
- Welded + Soldered connections (95/5 Pb/Sn solder)



# Burn-in / Life-test Configuration

- Configured for continuous conversion at  $V_{in}$ =half-scale
- Buffer Amp configured as voltage-follower with  $V_{in}$ =2.5V
- $V_{DD} = 6V$  (operating = 5V)
- Oven at 250°C



# Electrical Test Parameters

- At each electrical test point collected data using automated tester
  - On-chip temperature monitored by forward drop of ESD diodes
  - Test program collects DC data:
    - Buffer Amplifier offset voltage at 2.5V VIN
    - ADC offset, full-scale, and linearity errors
    - Conversion Time: Controlled by on-chip R-C oscillator
    - No-load output of the 2.5V reference
- w Conversion time and VREF tempco/scale-factor are trimmed at wafer test*

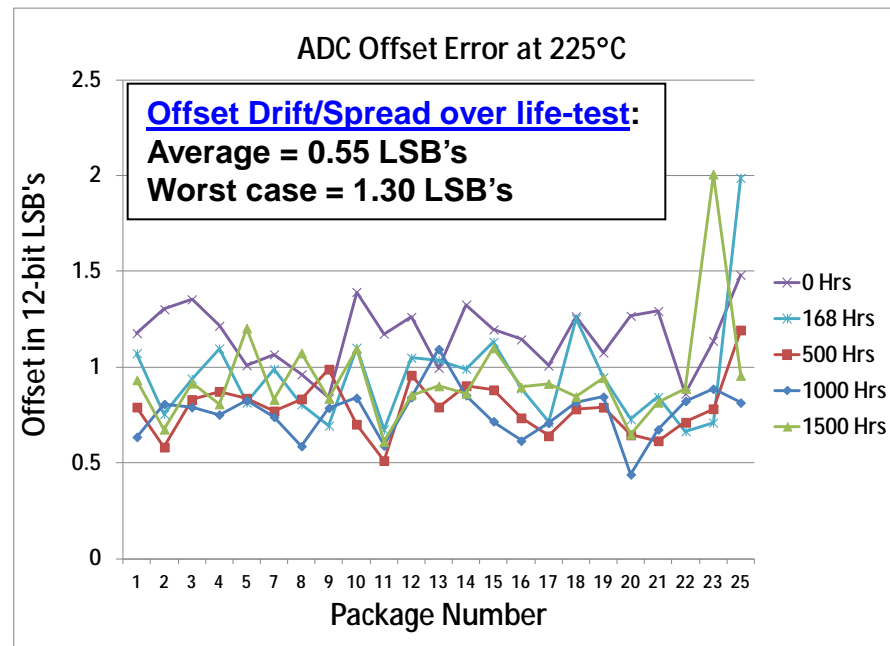
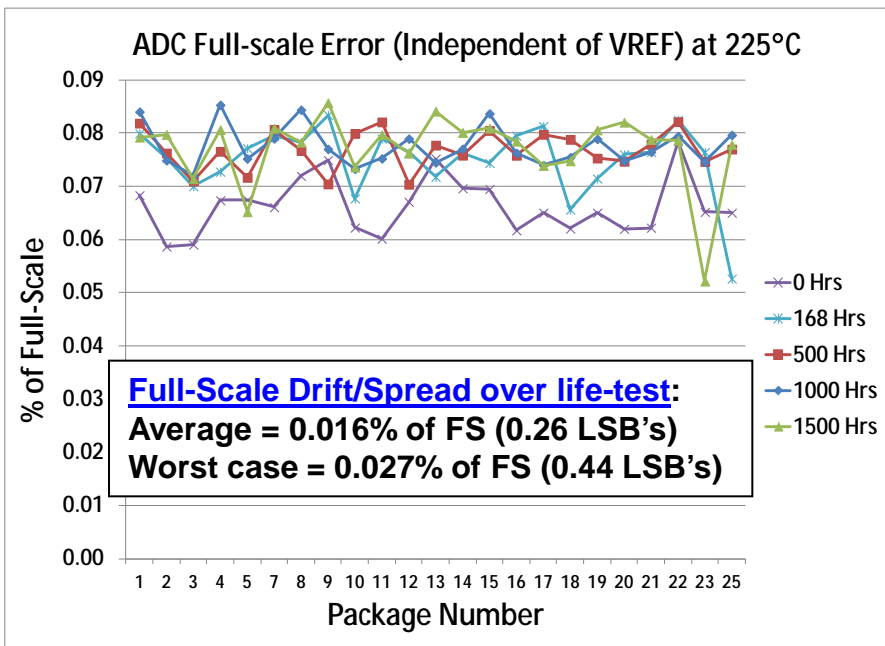
## Note:

- The ADC has superior INL/DNL performance at high temp relative to room temperature
- Cross-over from 1.1 to 2.0 LSB INL to 0.5 LSB INL is observed at »160°C
- This is attributed to design attributes rather than process/device stability

*225°C results provide best insight into performance and stability of the technology*

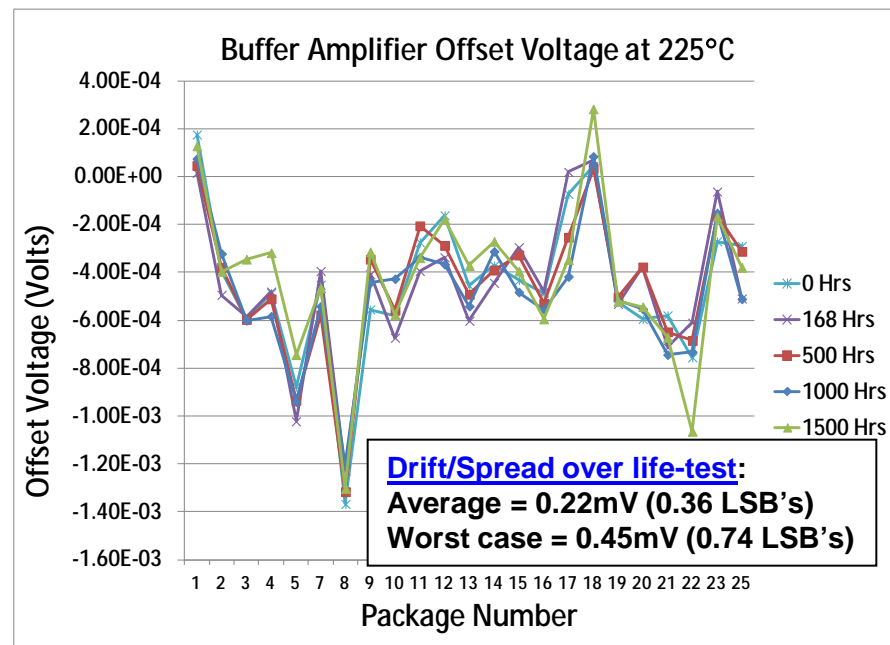
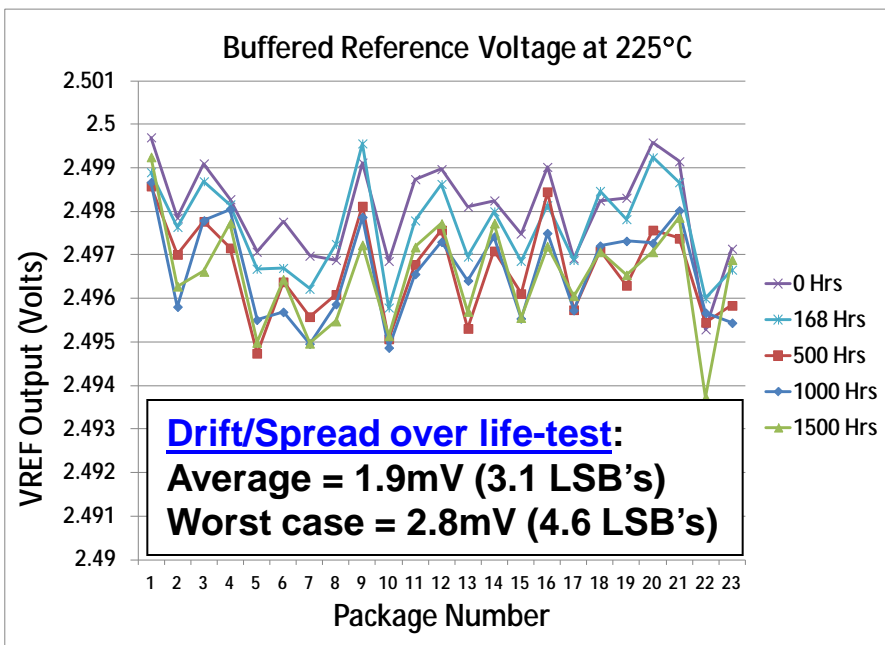


# Life-test results (225°C data)



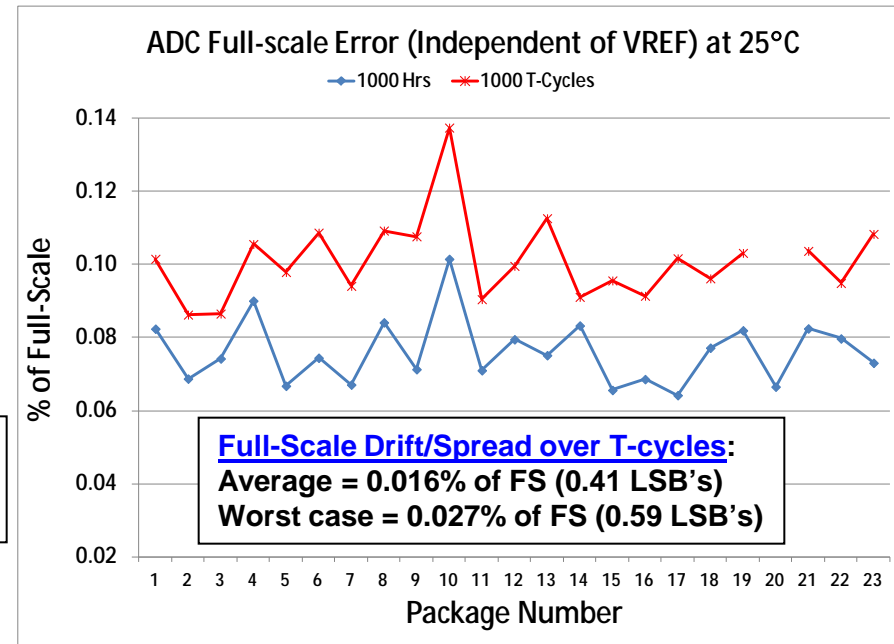
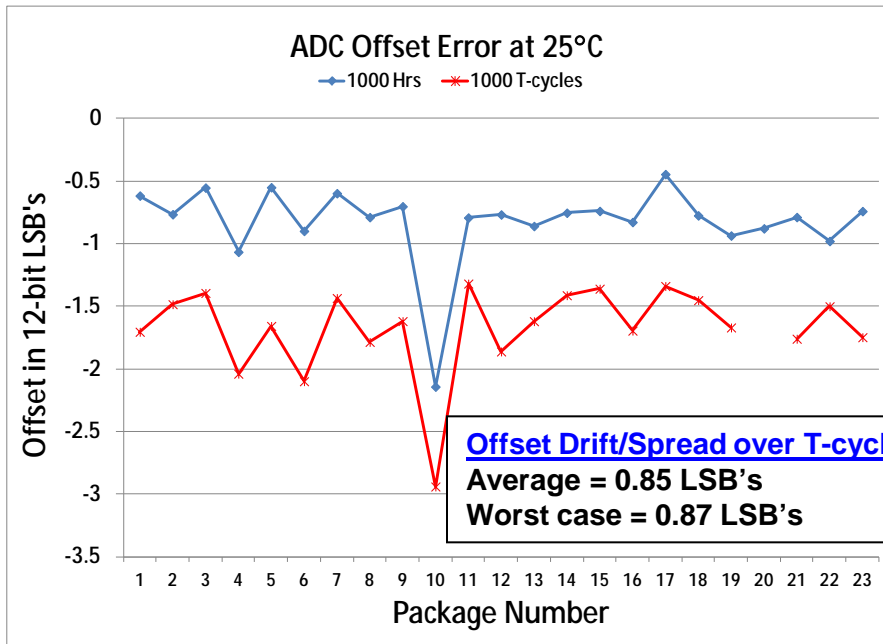
- These results are obtained with an external reference applied (i.e., independent of any VREF drift)
- General trend:
  - Full-scale/Offset errors show an initial shift (within 168 hrs) in opposite directions
  - Indicative of an “end-point shift” in the transfer function

# Life-test Results (225°C data)



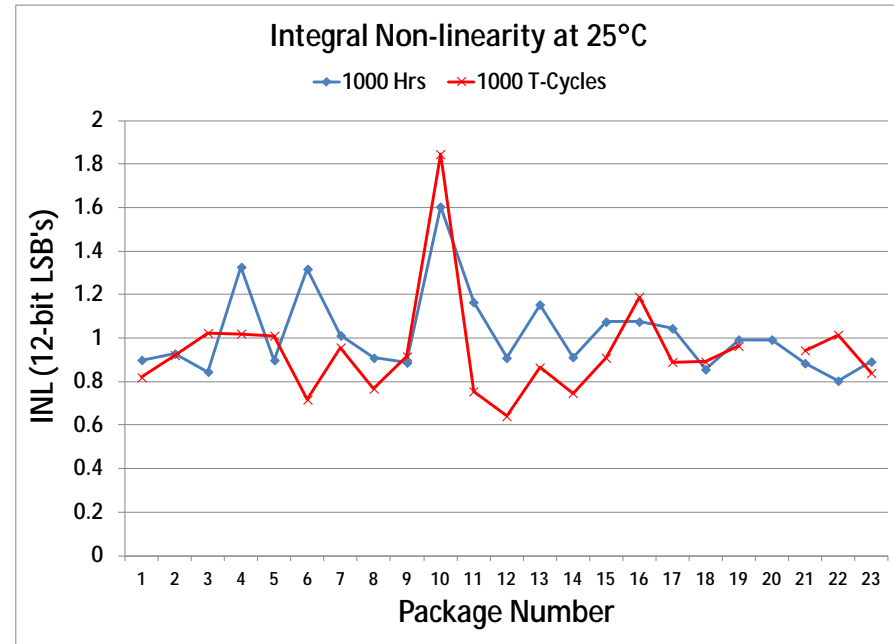
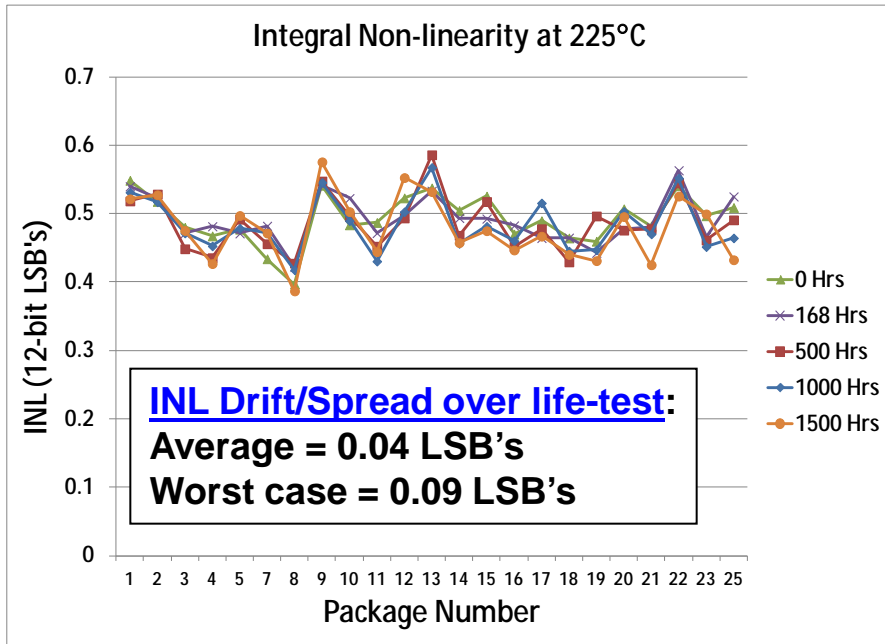
- **Buffered 2.5V reference is generally applied as the ADC Reference Input and defines the full-scale input range**
- **Buffer amplifier may be used to drive the ADC input**
  - **In that case shift in buffer amplifier offset adds to ADC offset**

# Temp. Cycling Results (25°C Data)



- Above charts compare data prior to T-cycling (blue) to data obtained after T-cycling (Red)
- Full-scale/Offset shifts in opposite directions are observed
  - Indicative of an “end-point shift” in the transfer function

# Integral Non-Linearity (INL) Results



- **1500 hours at 250°C + 1000 T-cycles does not significantly change linearity**

# Electrical Parameter Summary

Predicted Accuracy Degradation from Results			
	Typical	Worst-case	Units
<b>Drift after 1500 hrs @ 250C</b>			
ADC Offset and Full-scale	0.81	1.74	LSB's
Buffer Amplifier	0.36	0.74	LSB's
VREF	3.1	4.6	LSB's
<b>Additional Drift from 1000 T-Cycles</b>			
ADC Offset and Full-scale	1.26	1.46	LSB's
<b>Total from above sources</b>			
	5.53	8.54	LSB's
	0.14	0.21	% of FS

- Reference drift is dominant error source
- Followed by ADC Offset/Full-scale drift with temperature cycling
- Resolution/Linearity is not significantly impacted

# Mechanical / Assembly Test Results

- **All parts passed hermeticity tests**
  - Mil-Std 883, TM1014, conditions A1, C1
  - 1500 Hours at 250C, 100 Temperature Cycles (-65°C, 200°C)
- **Wire-bond pull tests passed**
  - Mil-Std 883, TM1011, condition D
  - 1500 hrs @ 250C, 1000 T-cycles
  - 2 packages, 70 wires pulled
  - Ave. pull-strength = 5.7 grams, Minimum = 4.9 grams
  - Pass criteria is 2.0 grams
- **Die-shear tests passed**
  - Mil-Std 883, TM1019
  - 2-die tested : 23.3 kgf / 30.2 kgf shear strength
  - Pass criteria is 1.0 kgf

# Summary and Conclusion

- **Testing has been completed to provide benchmark data/results for predicting ADC performance over time at high temp. with temperature cycling**
- **Mechanical integrity, functionality, and linearity are stable over the test conditions**
  - **1500 Hours at 250C, 1000 Temperature Cycles (-65°C, 200°C)**
- **Total compensated accuracy degradation is 5.5 LSB's typical (3.3mV for a 2.5V full-scale range)**
  - **Dominated by reference voltage drift**
- **Potential for marginal improvement from extended burn-in/pre-conditioning**

**Honeywell High Temperature Website**

**[www.hightempsolutions.com](http://www.hightempsolutions.com)**

Bruce Ohme

[bruce.ohme@honeywell.com](mailto:bruce.ohme@honeywell.com)

Plymouth, Minnesota USA